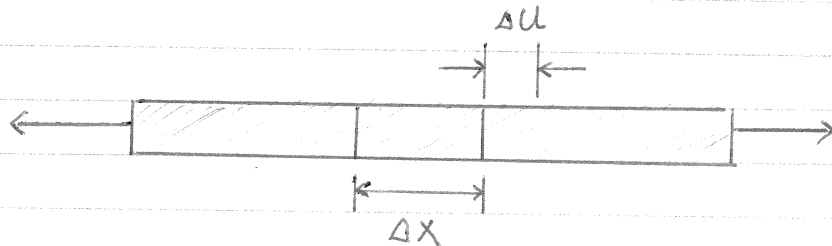


Strain (ϵ, γ) : measure of deformation.

basic definitions

Consider an element of material stretched in tension.
A section of length Δx is stretched by an amount Δu

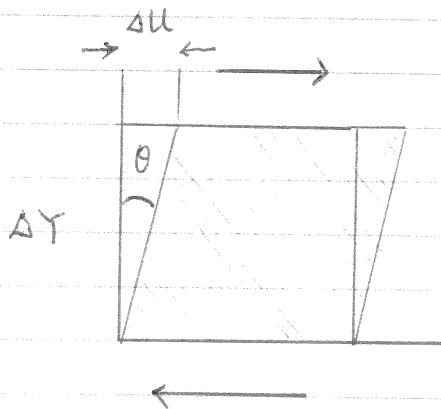


Infinitesimal strain at a point defined as

$$\epsilon = \lim_{\Delta x \rightarrow 0} \left(\frac{\Delta u}{\Delta x} \right) = \frac{du}{dx} \quad (\text{displacement per unit length})$$

↳ axial strain

The basic definition of shear strain is



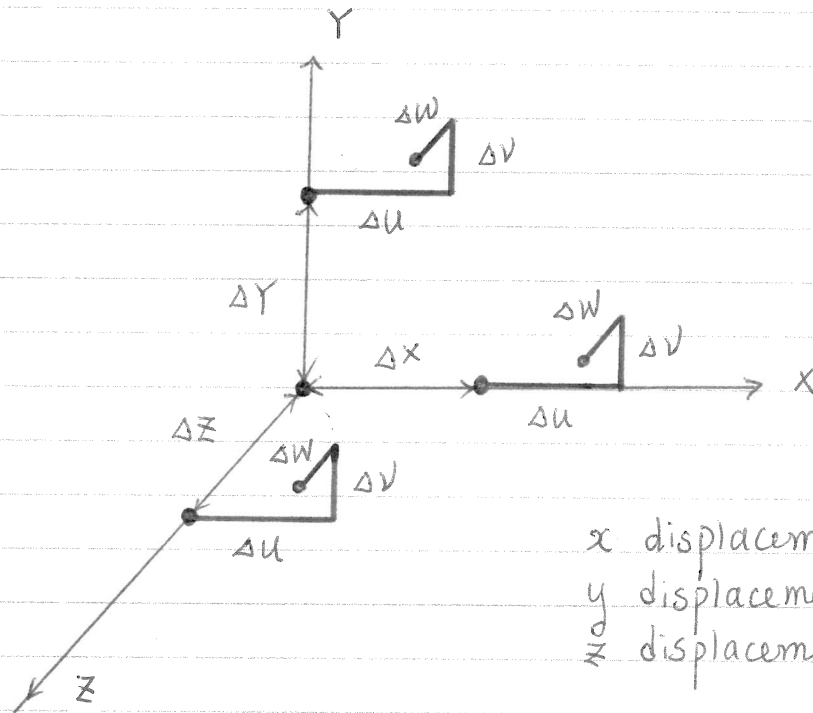
$$\gamma = \lim_{\Delta y \rightarrow 0} \left(\frac{\Delta u}{\Delta y} \right) = \frac{du}{dy} = \tan \theta \approx \theta$$

(displacement per unit length)

These simple definitions are OK only for very simple deformations.
We need a more general statement of strain at a point
to handle complex deformations.

Infinitesimal Strain at a point (3D)

Consider a Cartesian coordinate system imbedded in a solid which is to be deformed. Consider the relative displacements of the material points located on the axes.



$$\begin{aligned} x \text{ displacement} &= \Delta u \quad (\Delta u_x) \\ y \text{ displacement} &= \Delta v \quad (\Delta u_y) \\ z \text{ displacement} &= \Delta w \quad (\Delta u_z) \end{aligned}$$

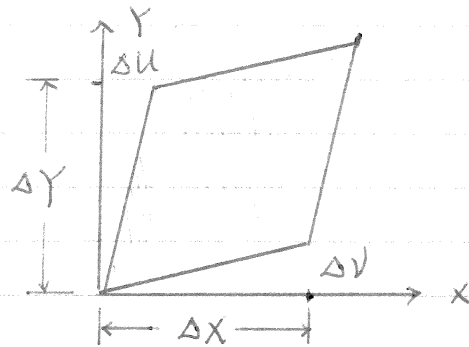
Axial strains :

$$\epsilon_{xx} = \lim_{\Delta x \rightarrow 0} \left(\frac{\Delta u}{\Delta x} \right) = \frac{\partial u}{\partial x} = \frac{\partial u_x}{\partial x}$$

$$\epsilon_{yy} = \frac{\partial v}{\partial y} = \frac{\partial u_y}{\partial y}$$

$$\epsilon_{zz} = \frac{\partial w}{\partial z} = \frac{\partial u_z}{\partial z}$$

Shear strains



$$\nu_{xy} = \lim_{\Delta Y \rightarrow 0} \left(\frac{\Delta U}{\Delta Y} \right) + \lim_{\Delta X \rightarrow 0} \left(\frac{\Delta V}{\Delta X} \right) = \frac{\partial u}{\partial y} + \frac{\partial v}{\partial x}$$

$$\nu_{yz} = \frac{\partial w}{\partial y} + \frac{\partial v}{\partial z}$$

$$\nu_{xz} = \frac{\partial u}{\partial z} + \frac{\partial w}{\partial x}$$

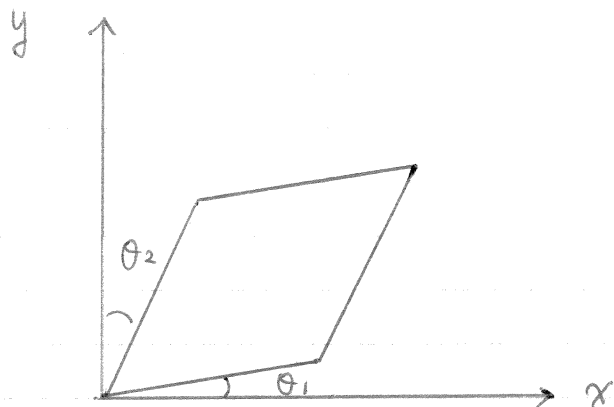
So, strain components can be described by a matrix

$$\text{strain} = \begin{pmatrix} \epsilon_{xx} & \nu_{xy} & \nu_{xz} \\ \nu_{yx} & \epsilon_{yy} & \nu_{yz} \\ \nu_{zx} & \nu_{zy} & \epsilon_{zz} \end{pmatrix} \quad \text{where } \nu_{xy} = \nu_{yx} \text{ etc.}$$

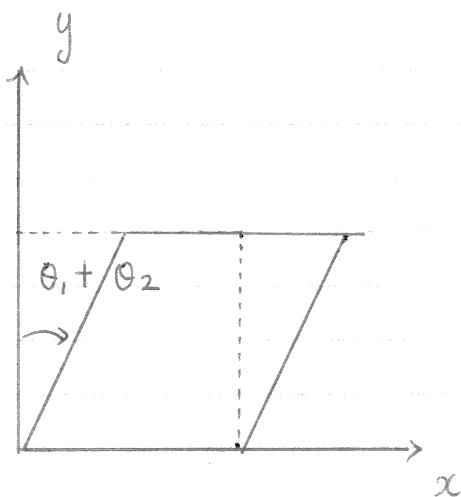
$$\text{strain} = \begin{pmatrix} \epsilon_1 & \epsilon_6 & \epsilon_5 \\ \cdot & \epsilon_2 & \epsilon_4 \\ \cdot & \cdot & \epsilon_3 \end{pmatrix}$$

These are called the engineering strain components.
They are used to define "elastic constants" of crystals.

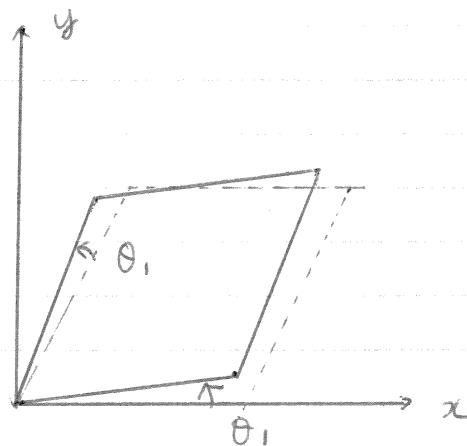
why $\tau_{xy} = \frac{\partial u}{\partial y} + \frac{\partial v}{\partial x}$? = $\theta_1 + \theta_2$



||



+



$$\tau_{xy} = \theta_1 + \theta_2$$



$$\frac{\partial v}{\partial x}$$

$$\frac{\partial u}{\partial y}$$

rigid body rotation

$$\omega_z = \theta$$

no contribution to the development of stress!

The Strain Tensor

For some problems in elasticity it is convenient to describe strain as a symmetric 2nd rank tensor.

$$\varepsilon_{ij} = \frac{1}{2} \left(\frac{\partial u_i}{\partial x_j} + \frac{\partial u_j}{\partial x_i} \right) \quad i, j = x, y, z$$

This gives axial strains as

$$\varepsilon_{xx} = \frac{\partial u_x}{\partial x} \quad \text{etc.}$$

but shear strains are

$$\varepsilon_{xy} = \frac{1}{2} \left(\frac{\partial u_x}{\partial y} + \frac{\partial u_y}{\partial x} \right)$$

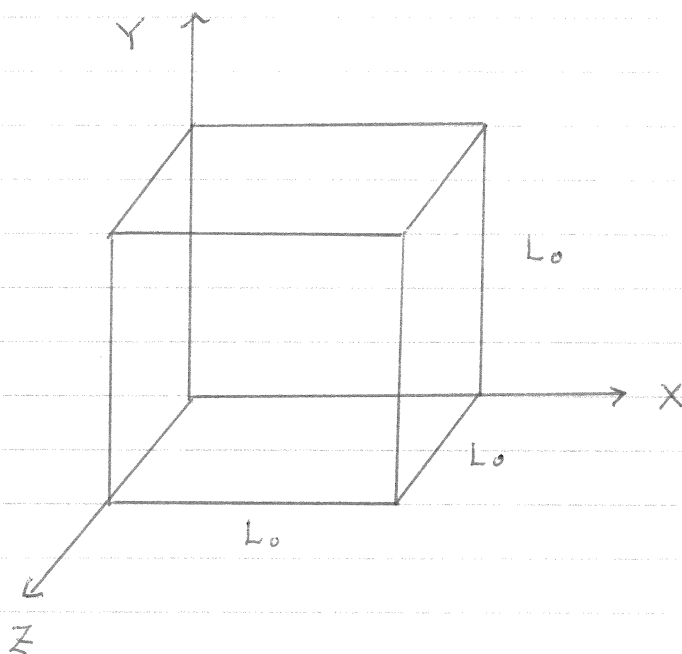
which is different by a factor of $1/2$ from above

The strain tensor can also be written as a symmetric matrix

$$\varepsilon_{ij} = \begin{pmatrix} \varepsilon_{xx} & \varepsilon_{xy} & \varepsilon_{xz} \\ \varepsilon_{yx} & \varepsilon_{yy} & \varepsilon_{yz} \\ \varepsilon_{zx} & \varepsilon_{zy} & \varepsilon_{zz} \end{pmatrix} \quad \varepsilon_{xy} = \varepsilon_{yx} \quad \text{etc.}$$

Note: transformation to different coordinate systems requires use of strain tensor

$$\text{Dilatation (volumetric) strain} = \frac{\Delta V}{V_0}$$



From the definition of strain

$$\begin{aligned} L_x &= L_0 (1 + \epsilon_{xx}) \\ L_y &= L_0 (1 + \epsilon_{yy}) \\ L_z &= L_0 (1 + \epsilon_{zz}) \end{aligned} \quad \left(\because \epsilon_{xx} = \frac{L_x - L_0}{L_0} \right)$$

Using these we can write

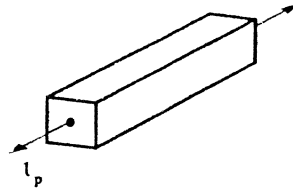
$$\begin{aligned} \frac{\Delta V}{V_0} &= (1 + \epsilon_{xx})(1 + \epsilon_{yy})(1 + \epsilon_{zz}) - 1 \\ &= \epsilon_{xx} + \epsilon_{yy} + \epsilon_{zz} + \underbrace{\dots}_{\text{high order terms}} \end{aligned}$$

Ignore the higher order terms (the assumption of small strain).

$$\Delta = \frac{\Delta V}{V_0} = \epsilon_{xx} + \epsilon_{yy} + \epsilon_{zz}$$

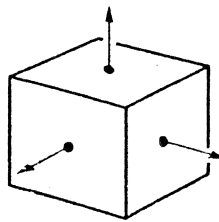
EXAMPLES

UNIAXIAL TENSION (ELASTIC)



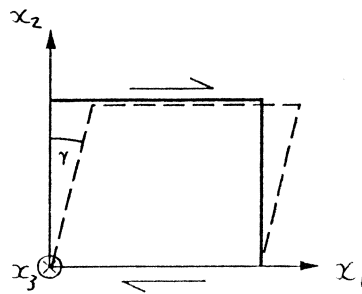
$$\varepsilon_p = \begin{pmatrix} \varepsilon_1 & 0 & 0 \\ 0 & -\nu\varepsilon_1 & 0 \\ 0 & 0 & -\nu\varepsilon_1 \end{pmatrix} \quad \text{and} \quad \Delta = \varepsilon_1(1 - 2\nu).$$

HYDROSTATIC TENSION



$$\varepsilon_p = \begin{pmatrix} \varepsilon & 0 & 0 \\ 0 & \varepsilon & 0 \\ 0 & 0 & \varepsilon \end{pmatrix} \quad \text{and} \quad \Delta = 3\varepsilon.$$

ENGINEERING SHEAR



$$e_{21} = \gamma \quad \text{and} \quad e_{12} = 0.$$

Thus

$$\varepsilon_{12} = \varepsilon_{21} = \frac{1}{2}(e_{12} + e_{21}) = \frac{\gamma}{2}.$$